

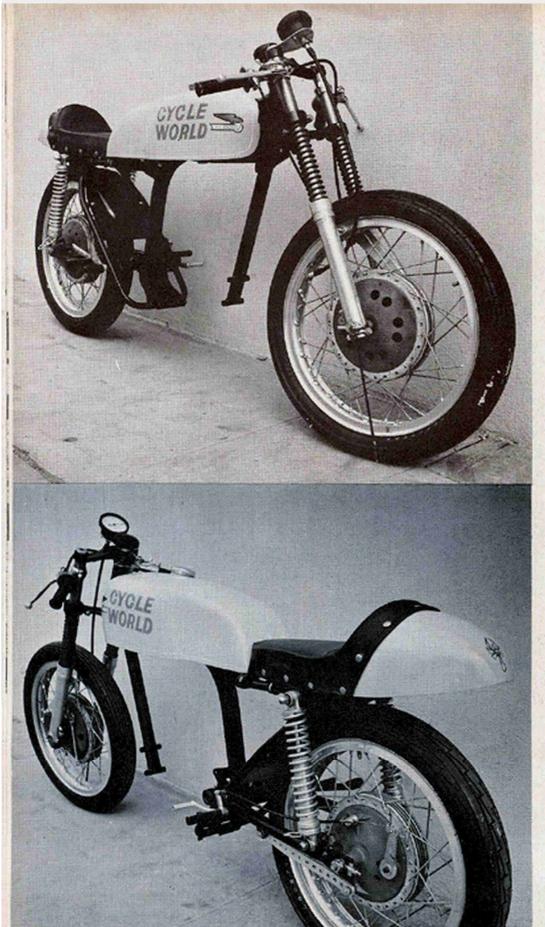
# DUCATI 250 FOR RACING

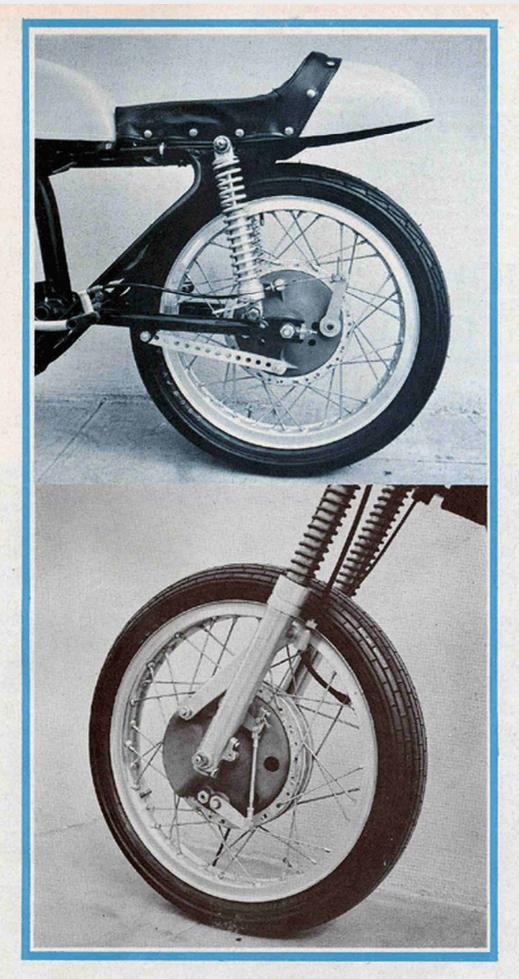
On the occasion of our road-testing the first 5-speed version of the Ducati 250, we remarked upon the bike's obvious road racing potential. Just fit clip-on handle-bars, a megaphone and racing tires, and you can have a low-budget bash at racing. Then, if you like the game, the Ducati always be further modified to make it more competitive. These thoughts came to us in the course of our test, and they must have occurred to many others, for the starting lineup in American road races will always include a flock of Ducatis.

However, it is a long, long jump from a good training machine to a race winner, and while it would seem on the face of it that the Ducati 250 has winning possibilities, not even the Ducati factory has produced one that will run with the Yamaha TD-1B and Harley-Davidson Sprint CR "production-racers." This should not be taken as criticism of the sportstouring Ducati. The 250-class has become ferociously competitive, and the Ducati is not the only otherwise-satisfactory touring 250 that has not been developed sufficiently to become a winner.

Around CYCLE WORLD's offices, the consensus of opinion is that the Ducati does offer the necessary scope for development into a competitive 250. But, opinion was not so optimistic as to obscure the undeniable fact that there is a lot of developing to be done. Therefore, when we actually started our Ducati-for-racing project, the first item on the agenda was a thorough investigation of the motorcycle, just to establish how much could be done with the engine and chassis. Work on the latter was necessarily restricted by the desire, on our part, to build a machine that would be "legal" for AMA Class C competition. Engine modifications, it was decided, should be held to those things available to our readers. We wanted a finished package that anyone, having access to basic machine-shop facilities and with moderate capital, could duplicate.

Our first step was to disassemble everything. Such items as the standard sent and fuel tank were disposed of immediately, being too heavy and otherwise unsuited for a serious racing effort. We would have preferred to discard the frame as well; it is also only slightly lighter than an anvil and a proper double-loop "duplex" frame would offer more rigidity at about half the weight. Unfortunately, the





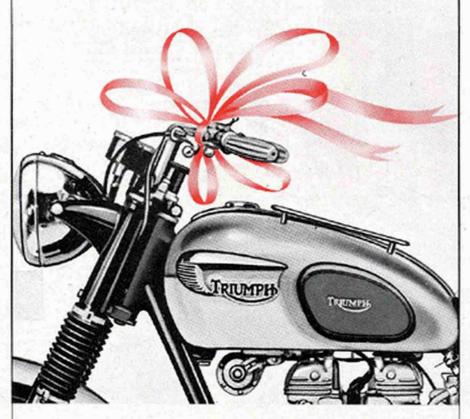
AMA's technical inspectors would probably not appreciate anything quite so enterprising as a special frame.

Initially, we had thought that some modification of the forks might be necessary, but a close inspection indicated otherwise. The damping characteristics appear to be just what is needed for road racing. The rear suspension's spring/damper units are another matter. People have used the standard units with fair success, but there are replacement ones available that give better results. Ducati makes a racing replacement (these are not always available), and the Italian Ceriani units distributed by Cosmopolitan Motors would do the job. Even so, the convenient selection in spring-rates made us decide upon Girling suspension units. These give virtually no damping on bounce, but a very strong action to restrain rebound, and that is, our experience tells us, exactly what is needed for road racing. We would prefer to fit these dampers with Girling's progressiverate 60/90 (60 pounds-inch initially, building to 90 pounds-inch at full compression) springs, but these are rarely in stock here in the United States. Lacking those progressive springs, we will start with straight 75 pound-inch springs. Rates up to 90 pound-inches will be tried, and it is anticipated that slightly stiffer springs will be used on fast, relatively smooth courses. Incidentally, the construction of the Ducati forks, which have external springs (we have removed the dust-covers from the forks so these are now exposed), permits experimentation with spring-rates up front. Actually, we do not think this will be necessary but it is nice to know that we have the option of changing the front springs.

About 6 pounds was trimmed from the standard frame by removing the foot-rest brackets and some surplus material around the back of the rear engine/swing-arm mount. More could have been eliminated by drilling holes in everything, but as this would have only amounted to another pound or two, at most, it did not seem to us to be worth the effort. Especially, this swiss-cheese effect looked unattractive to us because of possibly weakening the structure.

(Continued on page 74)

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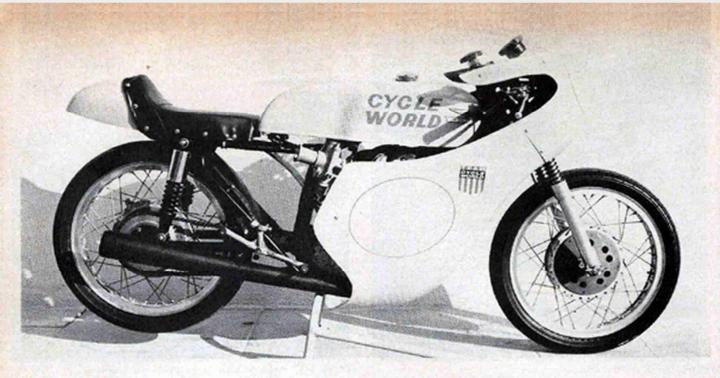
## **DUCATI** continued

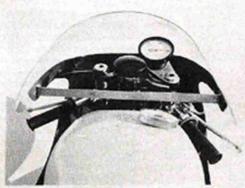
At present, the CYCLE WORLD Ducati still has its friction-type steering damper. In touring use, this is a good thing, lending stability over humps and bumps in the road surface. Racing is another matter. To get the desired delicacy of control, one must keep the friction damper quite slack; too slack, in fact, to be of much benefit. Where a damper is really needed is in recovering from a slide: the rear wheel steps-out, you correct, and when the bike straightens, its forks will flick right over on opposite lock. This results because "trail" yanks the forks back toward center, after which inertia carries them over near full opposite lock. Following this, they will again be swung back toward center and again inertia will over-do things for the rider. On a good handling bike, these oscillations lose amplitude with each successive cycle, and disappear without doing any damage (usually). Sometimes however, with even the best of motorcycles they will occur with such violence that the rider will be thrown off. The only damper capable of correcting this condition is the hydraulic type, which is velocitysensitive. Hydraulic dampers have no effect on small, low-speed steering oscillations, but they will prevent the forks from flapping. Before we try any serious racing, the friction damper will be removed, and a hydraulic damper substituted.

A lot of people have tried to make touring brakes do a racing job, and to the best of our knowledge, this has never been entirely successful. So, just to nip-off a budding problem, we ordered a set of Oldani brakes from Italy. These have 200millimeter (7.88-inch) drums, cast of magnesium alloy with riveted-in iron liners. The front brake has double-leading shoe actuation; the rear, single. A flange is provided for mounting the rear wheel sprocket but it is rigid, instead of the cushion-drive hub of the standard Ducati. To take shock out of the drive, a spring-hub Oldani sprocket is supposed to be used with the Oldani rear hub. We have another idea for the sprocket arrangement which will be explained next month. Cushion-hub Oldani sprockets are rare, and we are trying to use as many readily-available

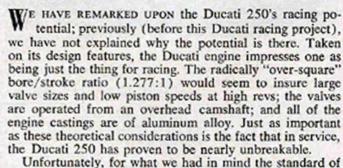
parts as possible. Clip-on bars, complete with control levers, can be obtained from Berliner Corporation, the Ducati Distributors, and we elected to use these. They are made to fit the bike and you won't find anything better. Fuel tank and fairing both came from Custom Plastics. The use of Goodyear road racing tires should not need explanation. Proper racing tires are absolutely essential, and our experience with the Goodyears indicates that they are at least as good in terms of adhesion as anything available. They are also somewhat expensive, but the wear-rate is so low that when one considers frequency of replacement, the Goodyear tires are a racing bargain.

This brings us to the end of the chassis modifications; at least, until testing indicates what other small changes will be needed. Next month, we will delve into the matter of engine work, which is a great deal more involved.



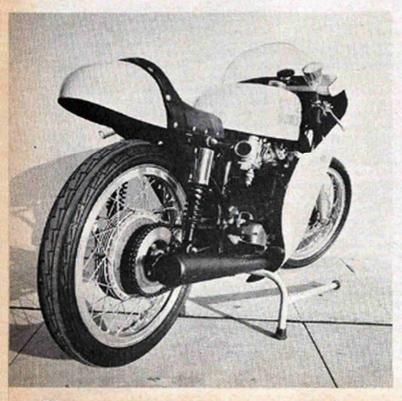


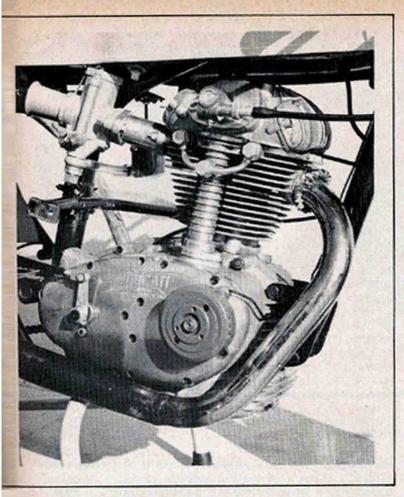
## A 250 DUCATI FOR RACING, Part Two



Unfortunately, for what we had in mind the standard of reliability established by normal (or even slightly abnormal) service was of limited value. It is axiomatic that maximum power will ultimately come from maximum revs, and our first task was to determine what order of crank speeds the Ducati was likely to withstand. Piston speed is one index of this; a better one is piston acceleration. This is calculated from stroke, connecting rod length, and engine speed. There is no fixed limit for piston acceleration, but considering that the Ducati has a good, forged piston, we tentatively placed our target limit at 125,000 ft/sec<sup>a</sup>. That limit is reached at just under 10,000 rpm, but because it is a somewhat elastic limit, the "red-line" our efforts would be directed toward was set at 10,000 rpm. The validity of this pencil-predicted limit is substantiated by the experiences of Frank Scurria, who has raced Ducatis with some success and who found a 10,000 rpm red-line to give reasonable reliability.

Once the upper limit was set, it then became a simple matter to determine the engine speed-range; this being calculated from the ratios provided in the standard Ducati





Only external evidence of engine modifications are oversize carburetor, special intake manifold and Stefa magneto flywheel.

5-speed transmission. To make the rather large jump from 1st to 2nd gear without dropping below the power band, power is required from 6500 rpm. However, on most race courses, one would not use anything under 2nd gear except on the start, so the real power band could be between 8000 and 10,000 rpm - that would cover almost any course and overall gearing conditions we would be likely to en-

Knowing how "peaky" power curves become in highly modified engines, we could estimate that with everything tuned for running in a 8000-10,000 rpm range the point of maximum output would be at about 9500 rpm. From that point, it was all fairly easy slide-rule work to arrive at an inlet valve and port size, and a diameter for the carburetor throat.

First to come in for consideration was the intake port diameter. This should be large enough to avoid throttling; yet, small enough to provide the gas velocity needed for good cylinder charging over a fairly wide engine-speed range. Experimental work has shown that gas-flow speeds in the order of 400 feet per second give good results, and a couple of racing engines have used even higher gas speeds. However, some degree of throttling occurs as the flow nears 400 ft/sec, and as we were dealing with a 5-speed transmission, it was not necessary to spread the power band very far. Therefore, we could settle for a narrower range and gain slightly in maximum power. Calculations showed that a port diameter of 1 3/16" would give us a maximum mean gas speed of 380 ft/sec at 10,000 rpm, with a minimum of 307 ft/sec down at 8000 rpm. The lower figure is still high enough to dampen the powerband narrowing effects of a moderately radical racing cam.

At the carburetor, there is no need for having more gas velocity than is necessary for proper air/fuel mixing. In fact, to maintain the high port-area gas velocities out through the carburetor is to incur entirely unnecessary flow losses due to friction. Our ultimate choice of carburetors, an Amal GP5 with 1 3/8" throat, gives a maximum flow velocity of 283 ft/sec; just high enough at 10,000 rpm to create some friction losses. More to the point, the flow at 8000 rpm is 226 ft/sec, which is low enough to make flow restriction minimal and high enough to give completely clean carburetion. Down at the 6500 rpm minimum, gas speed through the carburetor is only 184 ft/sec, and rather borderline for clean running, but accept-

Valve size was determined by the interaction of many factors. Contrary to some opinion, biggest is not necessarily best. Insofar as gas-flow is concerned, there is a point of rapidly diminishing returns with increases in valve size, and large valves are a positive embarrassment when dealing with long-overlap valve timing. Moreover, the big valves, which are always added mass in the valve gear, lower the point at which valve-float occurs. Finally, increased valve sizes mean bigger clearance pockets in the piston crown, and make it difficult to get a sufficiently high compression ratio.

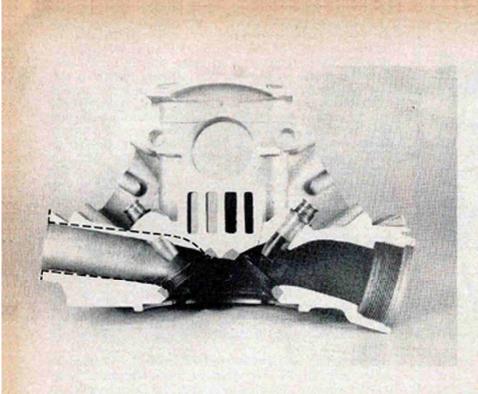
By juggling all of these factors around, we settled on an intake valve of 1 5/8" diameter, and a Matchless "twin" intake valve was selected to replace the Ducati valve. As a matter of fact, the latest Ducati 250s have an intake valve only a few "thou" smaller than 1 5/8" and the Ducati valve is made of excellent steel. Unfortunately, the Ducati valve is horribly heavy. The Matchless valve, with its smalldiameter stem and deeply tuliped head, is light and has a shape well suited to the port we were planning.

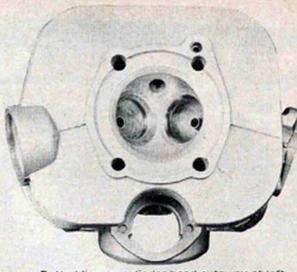
Ah, yes. The intake port. Here was where all the sliderule work came to a grinding halt and we embarked on a long and frustrating exercise in what is sometimes called "the art of the possible." In other words, making the best of a bad situation. Indeed, we did not fully realize how sticky the situation was until we sawed a cylinder head apart - cutting along the ports. The exhaust port is fine, but the intake port is, according to our Technical Editor, dreadful. While no doubt very easy to cast, being perfectly straight, it directs the gas flow across the valve head, and our tests indicate that only half of the valve circumference is effective to any worthwhile extent. An entirely new port shape would have to be carved into the cylinder head.

In the end, the job was done by milling a new port at 6-degrees downdraft (measured from the plane of the lower cylinder head face), to replace the original 9-degree port. The new port's upper edge starts at the upper edge of the original, out at the port mouth, but because it is slightly larger in diameter, the cut overlaps the bottom of the port. As the cutter moves in, it begins to remove material from the port roof, raising it about .250" above the valve. Hand-finishing (with rotary-files) created a pocket above the valve head to direct flow downward at the point, rather than diagonally across the valve.

All this lifting of the port roof improves flow, but it also brings problems. These originate from the scanty amount of material between the port and the valve-spring/rockerarm cavity. The port we have described breaks through into this cavity, and the break must be welded. Also, it leaves what may eventually prove to be too little metal around the valve guide, and this is rather poorly supported after the porting work is completed. Frankly, we fear that after some hours of running, the intake guide in our modified cylinder head may come adrift. If it does not, we will have gained a wonderfully smooth port. Should the worst happen, a boss to support the guide will have to be welded into the port.

It has become standard practice, when building a "hot"





Dotted line on cylinder head cutaway at left shows new port shape. Underside view of head above shows larger port blended into valve seat.

Ducati engine, to replace the stock hairpin springs with coils. Whatever inclination we might have had toward this was removed by the port shape used. To get room for coil springs, it is necessary to cut a relief in the spring-cavity floor at almost precisely the point where we had to weld on aluminum to close a breakthrough in the port roof. Thus, to get a good port shape, one must be prepared to use hairpin springs. As we have found, this is not the handicap it might seem. If the valve gear is light enough, the hairpin springs will do the job, and we had reduced the weight of our intake valve to only 53.9 grams - substantially lighter than a stock Ducati intake valve. (As a matter of interest, we used the original intake valve for an oversize exhaust valve, trimming it to 1 3/8" diameter. It is made of the same steel as Ducati's exhaust valves and was thereby suitable for its change of jobs.)

Machine-shop work, apart from the milling of the intake port, included making special valve-clearance caps, as the Ducati caps do not come in a size thick enough to work with the cam we used, and one had to be made to fit the smaller intake valve stem in any case. The camshaft is a Ducati part, and opens the intake valve 65-degrees before top center; closing it 75-degrees after bottom center. The exhaust valve opens 75-degrees before bottom center and closes 50-degrees after top center. Lift is .380" for the intake valve, and .360" for the exhaust. The valveclearance problem arises because the extra lift has been obtained by going to a smaller base circle on the cam.

We also machined an intake manifold. This part was machined from the solid, with a flange at one end to bolt against the head, and the other end flanged to match the carburetor. Length is 3" from face to face, as this spacing gave us the correct overall tuned-length for the intake tract. The manifold's bore is tapered from 1 3/8" to 1 3/16" between carburetor and port.

With the valve lifts and diameters we had, the pistoncrown clearance pockets were deep enough, but had to be made slightly larger. More depth might have been required, but we used the stock valve seats, and in cutting these for the bigger valves, we also moved the valves deeper into the head. Incidentally, the intake valve seat area was re-cut to give a large radius, or rolled effect, to improve flow when the valve is just off its seat. We might add here, too, that if you attempt to use larger valves than we have recommended, the piston's valve clearance pockets may become so large that there will be too little metal left

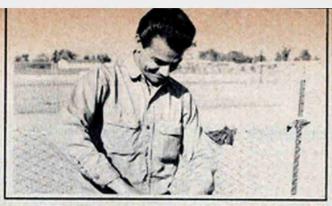
above the upper ring groove.

Little work is required down below the cylinder head joint. The stock piston was used, as it is a high-quality aluminum-alloy forging, and we did not feel that any of the alternatives offered any particular advantage. A higher piston crown would have been appreciated, as we lost some of the original 10.0:1 compression ratio by sinking the valves in the head, and cutting larger pockets in the piston crown. With those changes, the compression ratio drops to about 9.5:1 and we would prefer 10.5:1. In the future, we may machine the cylinder slightly shorter to move the piston farther into the head and boost the compression ratio up to the desired 10.5:1. A higher compression ratio would yield little gain in power, and with good breathing 10.5:1 will bring the engine near the point of detonation in any case.

One major modification we made that is not, in the strictest sense, entirely necessary, was to install a Swedishmade Stefa magneto. This unit is a standard fitting on the Greeves Challenger, and consists of a small rotor/generating coil/breaker-point assembly that feeds a low-tension output to a separate spark coil. Although primarily intended for two-strokes, it has been used on 4-stroke engines, and its performance in both types of engines has

been outstanding.

To install this magneto, we machined a new shaft to replace the one that normally drives the point-breaker cam in the Ducati. The new shaft extends out past the timing case, and the magneto rotor is fixed to a taper at the shaft's end. The magneto's point plate fits into the recess provided for the stock point plate — after the recess is machined to a slightly larger diameter. We added a sleeve just behind the recess, and it holds a ball bearing that supports the shaft. With the added load imposed by



Smiling Frankle Scurria, still recovering from his 1965 Daytona injuries, now serves as CW's builder/tuner/mechanic and worked on much of the Ducati.

the magneto rotor, we did not think that the original brass bushing would be up to the job. The bearing chosen is one with a seal on one side of the races, and this keeps the oil inside the timing case. The most difficult part of this whole conversion was in designing and machining a breaker cam right on the rotor shaft. There is not room to graft-in a breaker cam borrowed from something else.

Two reasons dictated this change. First, we could not use the Ducati magneto because its generating coil does not move with its points, and the points must be set to match the moment of maximum flux in that coil, rather than to whatever moment the engine might prefer for ignition. Thus, it is not possible (or at least not conveniently) to experiment much with spark-lead settings. Most "tuners" work around this by using a constant-loss battery/coil ignition, removing the Ducati generating coils and magnetic flywheel entirely. This works well, but at the expense of carrying a heavy battery — which is also a potential troublespot; battery plates sometimes disintegrate due to vibration. Also, a battery/coil system does not match the high-revs performance of the Stefa magneto, nor does it match the magneto's high rate of voltage rise, which makes for great resistance to plug fouling.

The only other modification made below the cylinder head was in the transmission shifter-mechanism. We installed a Sturtevant ratchet-fork, as the older Ducati forks will bend sometimes if the rider attempts to hurry shifts.

Before starting this project, we had the Ducati engine dynamometer-tested, and the results were a bit surprising. With megaphone in place, and after setting the spark and changing jets, to get maximum output, we found ourselves with an honest 22.2 bhp at 8500 rpm. There must be something very special in the air around the Ducati factory's dyno room, for they claim 28 bhp, net, at 8000 rpm (at those revs, our engine delivered 21.3 bhp.) It becomes even more curious when one considers that the Ducati Diana is one of the fastest stock 250s, and virtually all of Ducati's competitors claim much more than 22 bhp. Is it possible that somebody, or several somebodies, has been playing fast and loose with the truth?

There is, at present, no way for us to know how much power we have obtained. The dynamometer facility originally used is currently being renovated, and we do not feel that it would be fair to use other facilities—where we are not certain of accuracy. But, on the basis of such comparative tests as we have made (measuring the CYCLE WORLD-Ducati's performance against the Technical Editor's Yamaha TD-1B), it would appear that we have that 30 bhp and perhaps a bit more. And, we have that wide spread of power. The engine is strong from 6500 rpm right to 10,000 rpm and beyond. It will go all the way to 11,000 rpm without separating, and without a trace of valve float. However, we do not expect that 11,000 rpm could be used very much without suffering a very nasty engine explosion.

Something we did not expect, but are delighted to have, is phenomenally easy starting. Most of our local races are held under FIM rules, with push starts, and if the Ducati does nothing else, it will be first at the first turn. When warm, you take three steps, hit the saddle and drop in the clutch. Invariably, this is followed by an explosion of exhaust noise and a rapidly disappearing motorcycle and rider.

Handling is good, though not outstanding, but the brakes work to perfection. Little pressure at the controls is needed to scrub off speed at a tremendous rate. With this, and the good low-speed pulling qualities of the engine, we expect that our Ducati will be quite a good short-course motorcycle. To make it effective on fast circuits, more sheer horsepower will be required, and we cannot, frankly, afford time for the prolonged development work needed to get that power. The amount of power needed would be in the order of 35-37 bhp, and to get that it will be necessary to direct efforts toward a power peak at probably 10,500 rpm, with the red-line up at 11,000. Reliability at that crank speed will not be good enough using a completely standard crank, rod and piston assembly. It can be done, however, by someone who can afford the time to find ways to keep the engine together while using 11,000 for long periods, and to develop a camshaft to give the horsepower.

At present, we have about 200 man-hours of time invested in the Ducati, and at retail prices (we won't try to kid you; we get a discount on most of this stuff) the CYCLE WORLD-Ducati road racing motorcycle would represent an expenditure of slightly more than \$1700. Before the bike reaches winning form (fast enough to compete on an equal basis with the Yamaha TD-1B, Harley-Davidson Sprint CR, or the new 250cc Bultaco TSS) we can envision that price being doubled. Presumably, the Ducati factory could afford this development cost; CYCLE WORLD magazine most definitely cannot afford the sheer number of hours involved — even though some individual enthusiasts can, and probably will.

What we hope we have done is to lay the groundwork for the above-mentioned enthusiasts. All modifications have been purposely held to things the individual can do, and we have given what we consider to be a good basis for further development. With this machine, we have demonstrated that a 1 3/8" GP carburetor works fine; that the stock valve springs do likewise; that you can get a good port carved into the head; and that the engine is quite safe up to 10,000 rpm without bearing, piston or valve-gear problems. From here on, it is every man for himself. It should be mentioned that the wet weight of the bike, complete with fairing, is 233-pounds, or 10-pounds less than the Yamaha TD-1B and probably 40-pounds less than a Sprint CR. Moreover, with a special frame (now possible under the AMA's rules) the Ducati's weight could probably be trimmed another 15-pounds and the handling improved. There is hope, Ducati Lovers; stay with it.

#### CYCLE WORLD-DUCATI ENGINE MODIFICATIONS

Compression ratio 9.5:1
Intake valve diameter
Exhaust valve diameter
Intake tuned length
Exhaust tuned length
Megaphone
Intake port diameter
Intake port angle 6-degree downdraft
Exhaust port standard
Valve timing, intake
Valve timing, exhaust
Ignition Stefa magneto
Ignition lead 40° Sturtevant shifter-fork
Carburetor Amal GP5
Remote float-chamber
Main jet

SPECTATORS at the recent Willow Springs

ACA races were treated to a rather strange sight - a single-cylinder fourstroke 250 breaking up the usual parade of Yamaha TD-Bs! Closer inspection revealed it to be the CYCLE WORLD Ducati, ridden by Ralph LeClerg, who has been 175 AFM and ACA champion on a Ducati for two years.

Ralph has purchased CYCLE WORLD's portion of the machine and is carrying on with the development where we left off. Several changes have been made: the Stefa magneto is replaced with a wet cell battery. Ducati ignition points and coil. The system now is the common Ducati total loss racing equipment, completely reliable and very efficient. It is impossible to find fault with this method of obtaining spark, unless one forgets to re-charge the battery. One very definite advantage is that considerable rotating weight has been eliminated, and although the battery weighs more than the magneto, it is "sprung weight" and means nothing in the total picture.

Some changes have been made to the cylinder head. Most drastic was to use longer valves of the same type, and install Webco coil springs, thus eliminating the critical, borderline condition found in the standard hairpin springs at 10,000 rpm. The inlet port had to be built up in the region of the valve guide to give more support to the guide. When port was originally enlarged, machining cut through into the rocker cavity. Two heliare repair jobs did not cure the tremendous smoking problems, due to oil leaking into the port when the engine had warmed up.

The welds failed for two reasons. First, if the port shape is to remain the same, it is necessary to remove most of the weld from the inside. Not much can be left in the rocker box, as the springs occupy most of the available space. The result is that although a repair has been carried out, there is still precious little to steady the guide, and stresses set up at high engine speeds will simply cause fatigue and lead to further cracking in this thin area.

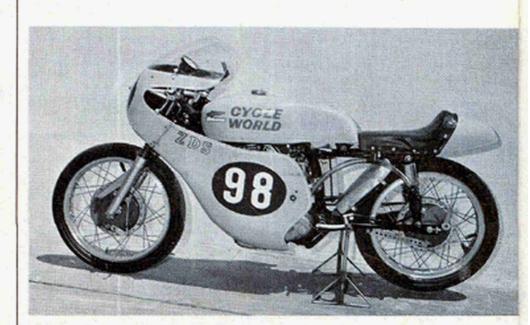
Valve guide movement was traced quite easily through chatter marks on the valve seat, although the engine had run for only a short period at moderate revs, where valve float would have been impossible. To cure the problem it was necessary to leave considerable meat around the guide and streamline the "lump" as much as possible. In addition, an oversize guide was fitted, as the previously mentioned movement had enlarged the guide hole.

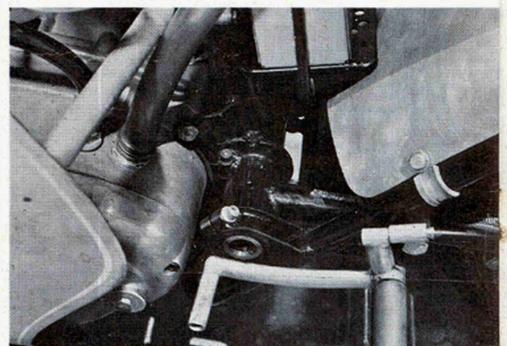
The piston is still the original part giv-

ing a compression ratio of slightly less than 10:1. Ralph feels, through experience with the 175 engine, that 11.1 will give better results, and this is the only other actual engine modification he has in mind at this time. Also, it has been found in the past that the oil pump will supply more

oil to the valve gear than can drain back to the sump through the standard drain lines when the engine is still cold. This is not a problem on street machines, where the engine is warmed up before high engine speeds are reached. However, it is a factor to be considered on an outright

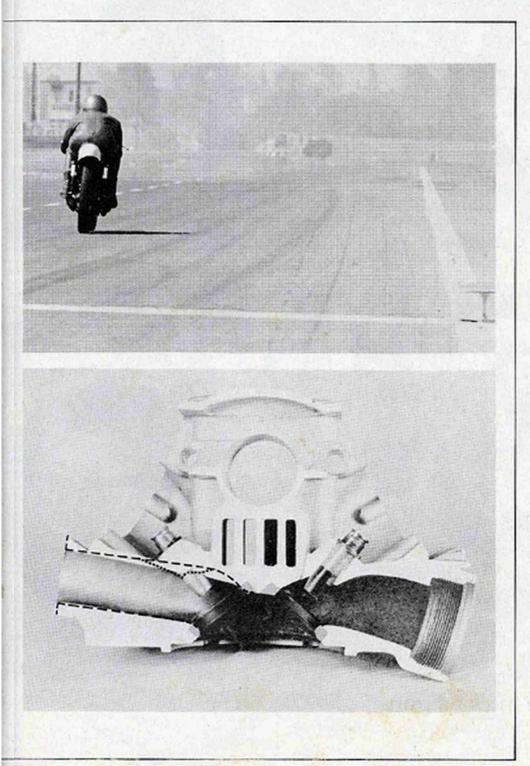
## A 250 DUCATI FOR RACING





racing engine warming up at four or five thousand rpm, as the over-abundance of oil in the rocker box can lead to oil leaking past the valve, until the oil is warm and good drainage begins. To compensate, an extra drain line has been installed on the left side of the engine. Ralph and the CYCLE WORLD expert on road racing feel that good handling can always offset a few horsepower. They feel, and rightly so, that there is no point having extra power if you can't use it. Because of this feeling, the major modifications to the machine have developed.

### PART THREE



A new swing arm pivot has been made from 4340 chrome moly steel, having a wall thickness of 1/8 inch, and extending to the full width of the rear sub frame down tubes. Short pieces of tubing, with inside diameter to match the new pivot, were welded to sheet metal mounting tabs. A lug was then welded to the tubing, and after saw-cutting through, the lug was drilled and tapped to use a 1/4-20 clamp screw. Then each assembly was pushed on to the protruding ends of the extra-long pivot, which acts as a jig, while the tabs are tack-welded to the rear down tubes.

While this modification is not worthwhile on a street machine, it is an inexpensive, completely satisfactory way to cure many evils, when the extra demands of increased horsepower and bumpy race courses are placed on a touring frame.

To ensure swing arm rigidity, large gussets have been added, which occupy all the space not required by the rear tire when the chain adjusters are at their most forward position. The .080 thick gussets are also made from 4340 and heliare-welded to the swing arm. While a few-pounds have been added to the frame, again it is sprung weight and of little consequence, as the lap times have proven.

Dynamometer testing is planned, but to help evaluate possible performance gain, we took the Ducati to Riverside for some timed runs and were pleasantly surprised to find considerable increases over a standard MKIII. In the standing 1/4 mile we reached a creditable 92.24 mph in 14.29 seconds, and a top speed of 116.12 mph. In standard trim the machine had done 80.5 and 16.3 seconds in the 1/4, while the top speed was 97 mph.

With the available horsepower before frame modifications, the 100 mph "sweeper" was a bit of a handful at Willow Springs, with plenty of jumping about, This means, unless one wants to go on his head, the engine cannot be used to maximum advantage. Yet, with the frame changes, Ralph was able to gain considerable ground on his opponents through this bend.

Of course, nothing is certain in racing. Ralph had fourth place all sewn up after a bad start, even passing and holding off John Buckner. Then, at two-thirds distance, the zipper on his new leathers came undone and a pit stop put him dead last. Lapping at the same speed as the leaders, he pulled back up to fifth place, just behind Buckner. In his quiet, unperturbed way, Ralph is getting a "thumper" into the hornet's nest.